

Development and Validation of a Radiance model for a Translucent Panel



Photo



Radiance

Christoph Reinhart, Maryline Anderson

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supported by:



National Research
Council Canada



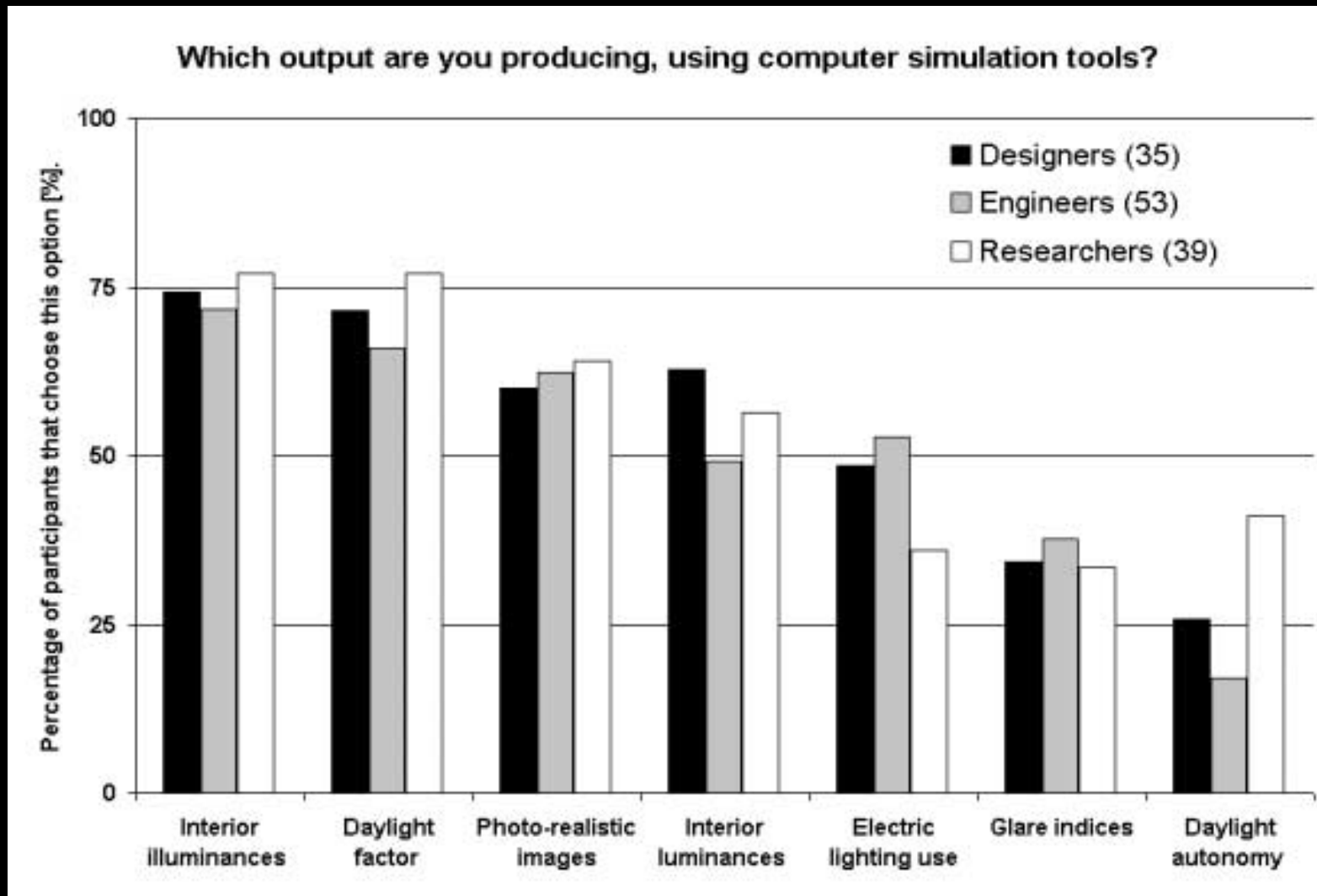
Outline

- Online survey on Daylight Simulations
- Previous Radiance Validation Studies
- Translucent Panel Validation
 - Goniophotometer/ Integrating Sphere Measurements
 - Development of a Radiance Material Model
 - Material Model Validation
 - Practical Considerations
- Conclusion

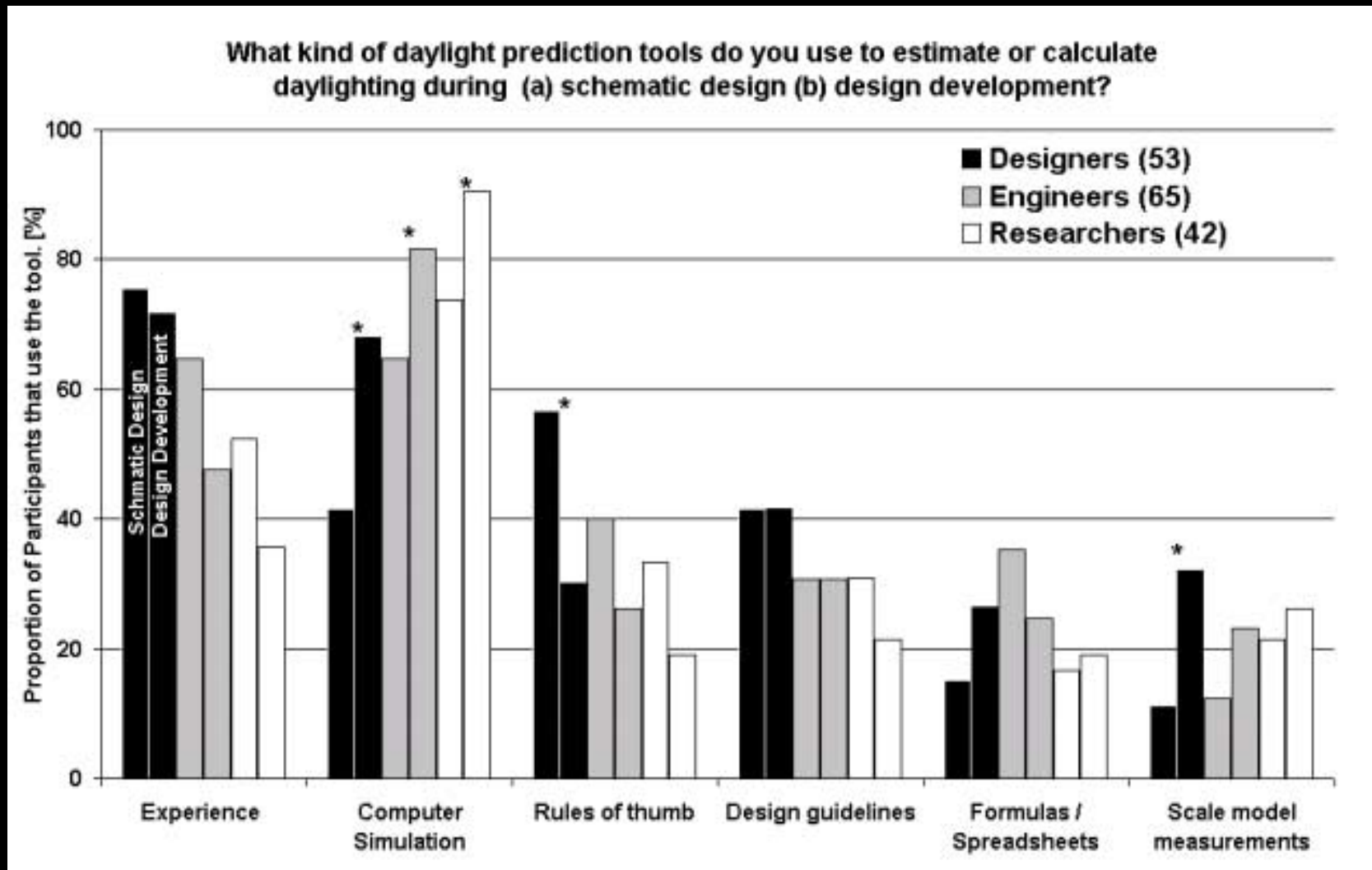
Survey on the current use of daylight simulations during building design

- online survey (January 2004)
- 185 individuals from 27 countries – 20% from Canada, 20% from the United States
- “*out of 40 selected tools, over 50% of votes went to Radiance*”
- sign up for a copy of survey results if you are interested

Simulation Output



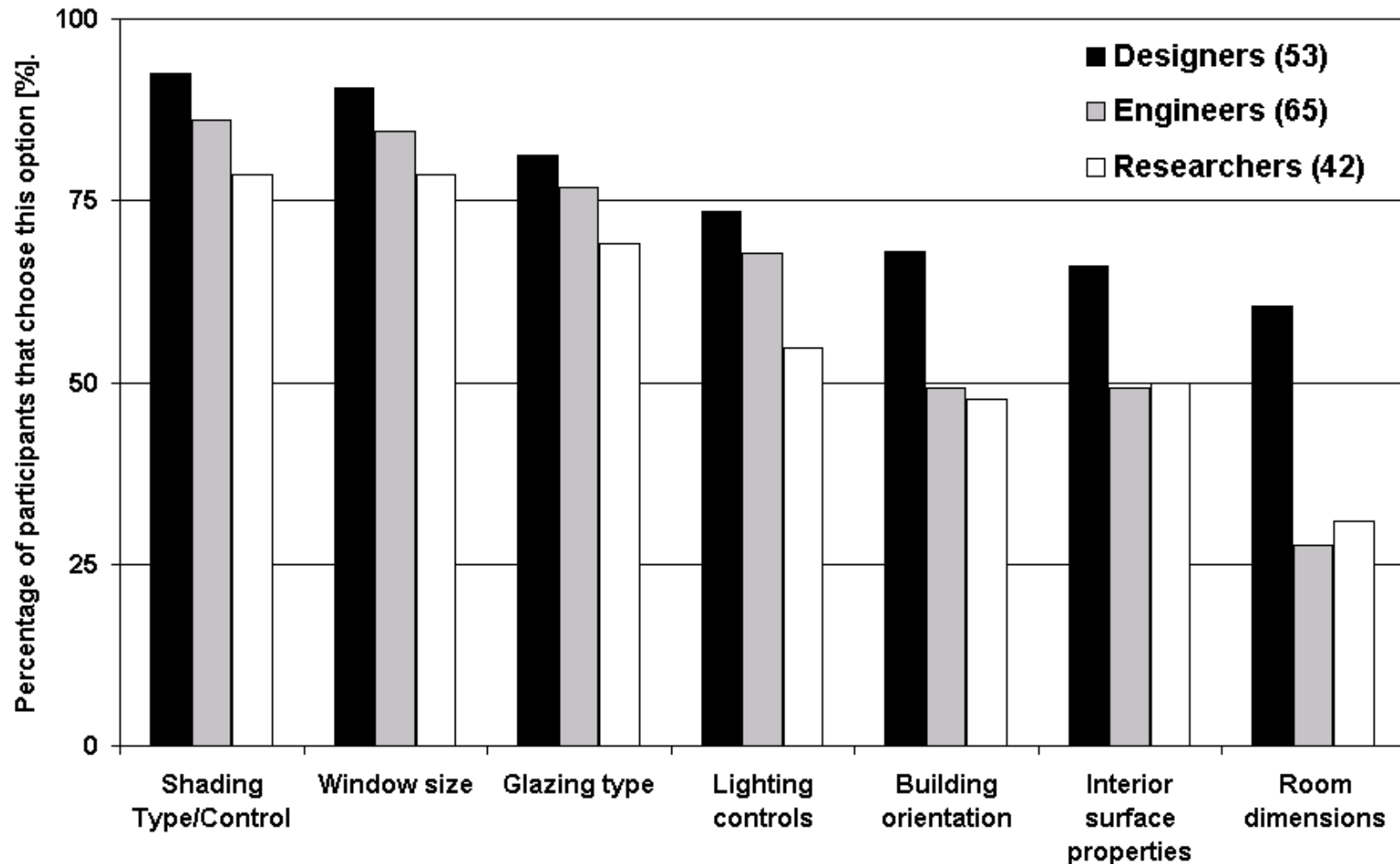
Prediction Tools Used



Increased use of simulations during design development... less use of scale models... digitalization is a general trend in building design.

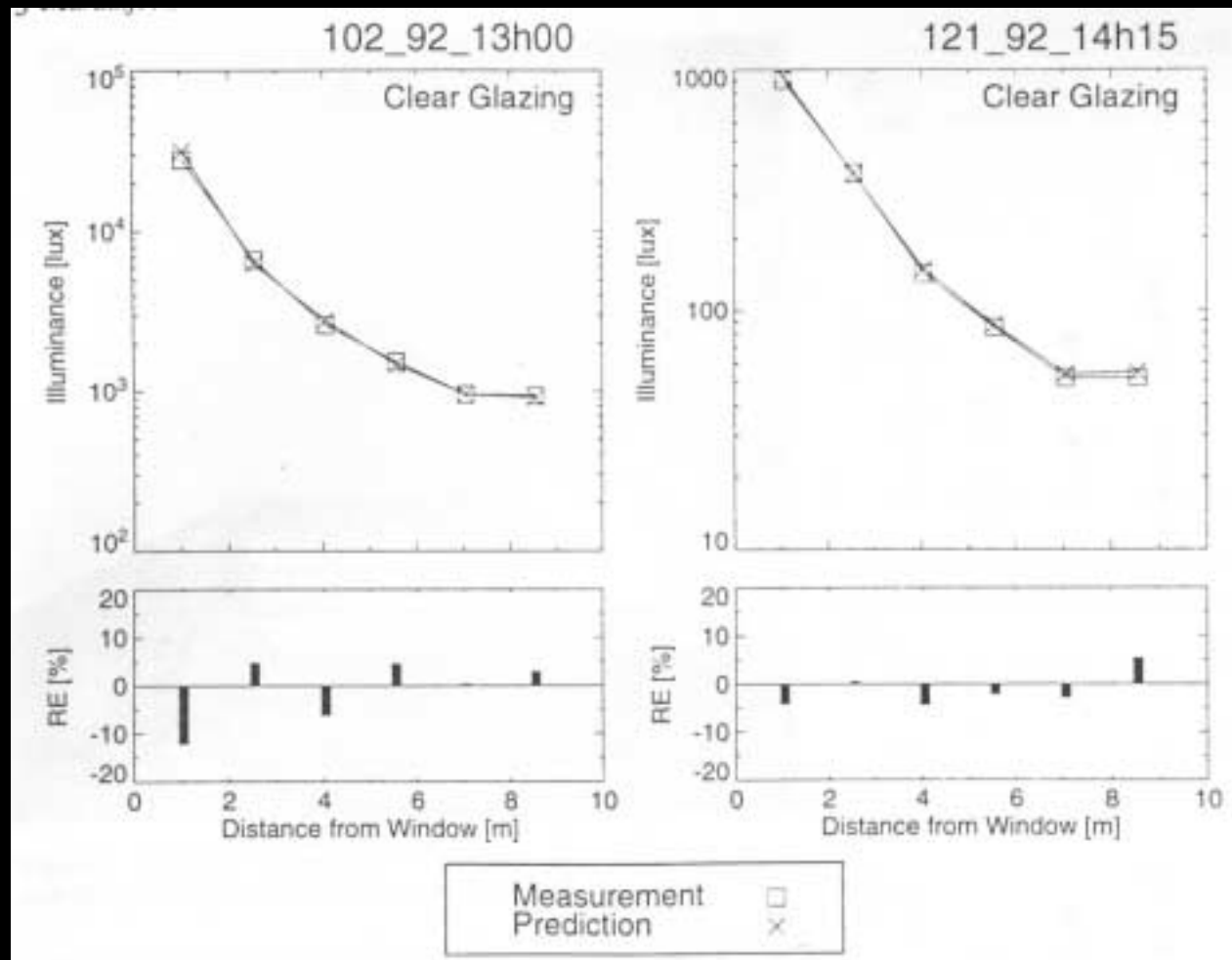
Effected Design Parameters

Which aspects of your design are affected by your daylight analysis?



Previous Radiance Validation Studies

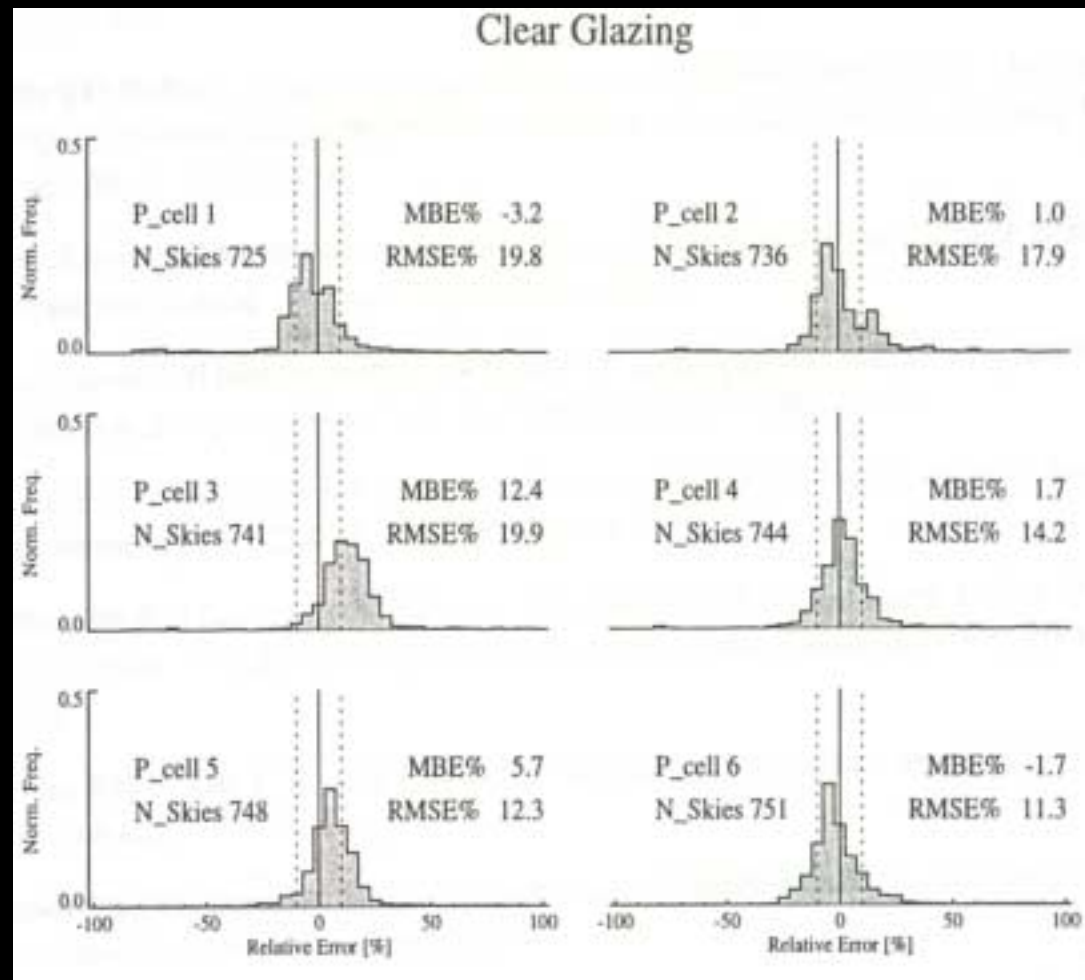
Light. Res. & Technology
Mardaljevic, 1995



Validation Radiance/ sky scanner data for a clear glazing with/without a lightshelf (Radiance materials: "plastic", "metal", "glass")

Previous Radiance Validation Studies

Light. Res. & Technology
Mardaljevic, 2000



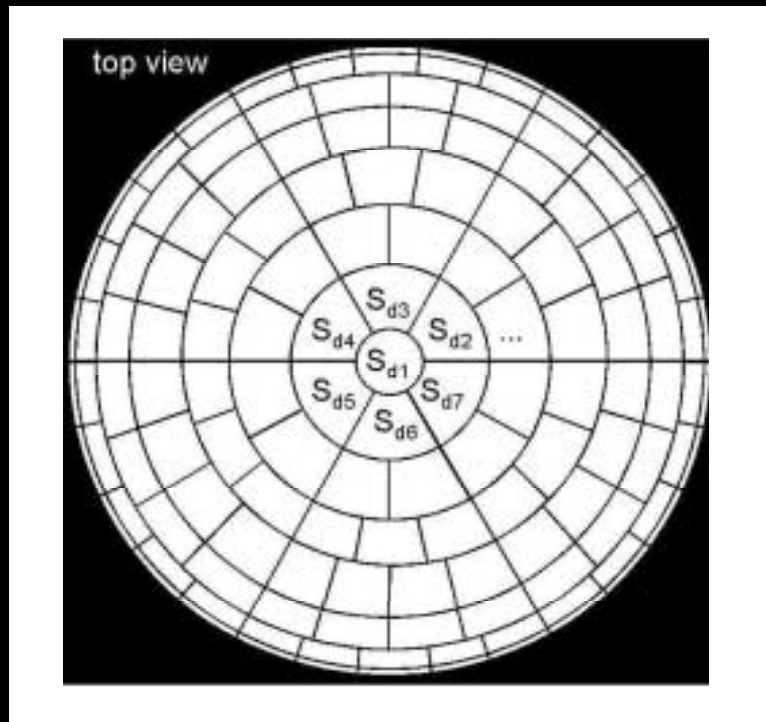
Daylight Coefficients: "same accuracy as standard Radiance"

(Radiance materials: "plastic", "metal", "glass")

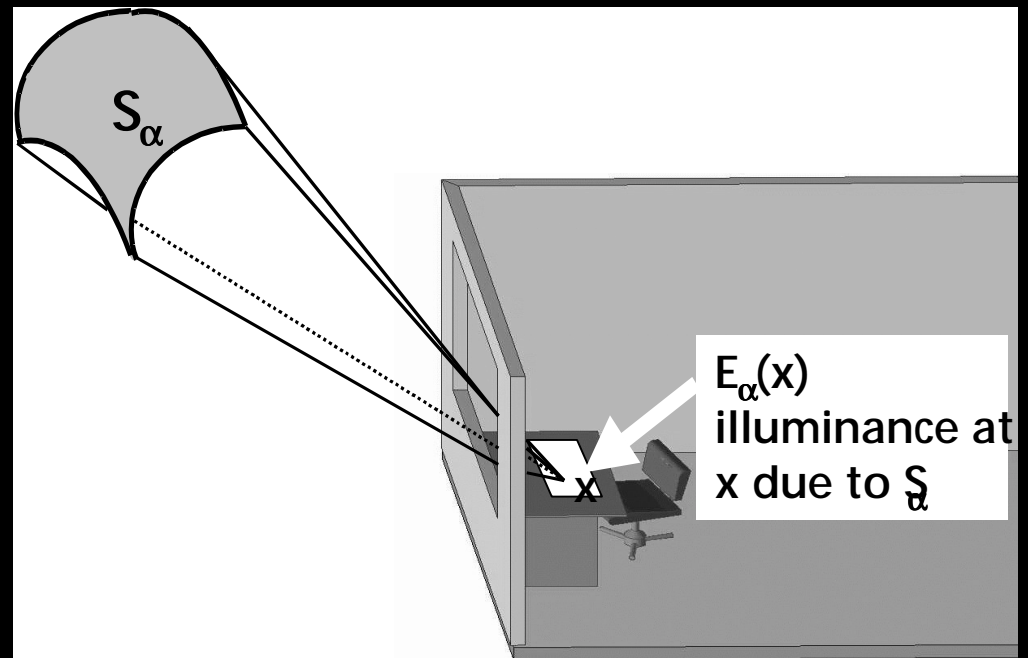
ARC-CARC

Daylight Coefficients

(1) Division of the Celestial Hemisphere



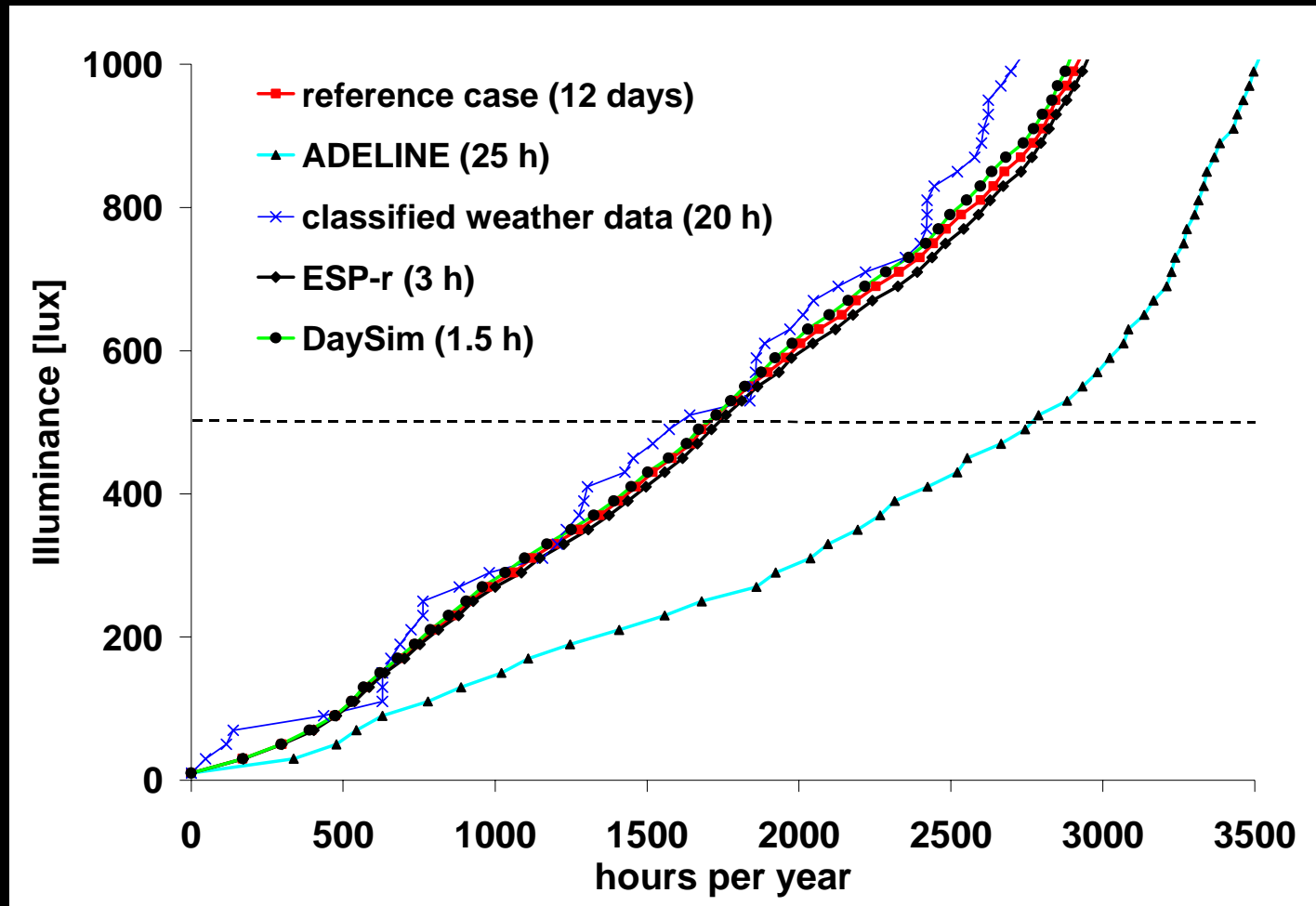
(2) Calculate Daylight Coefficients



Previous Radiance Validation Studies

Energy & Buildings

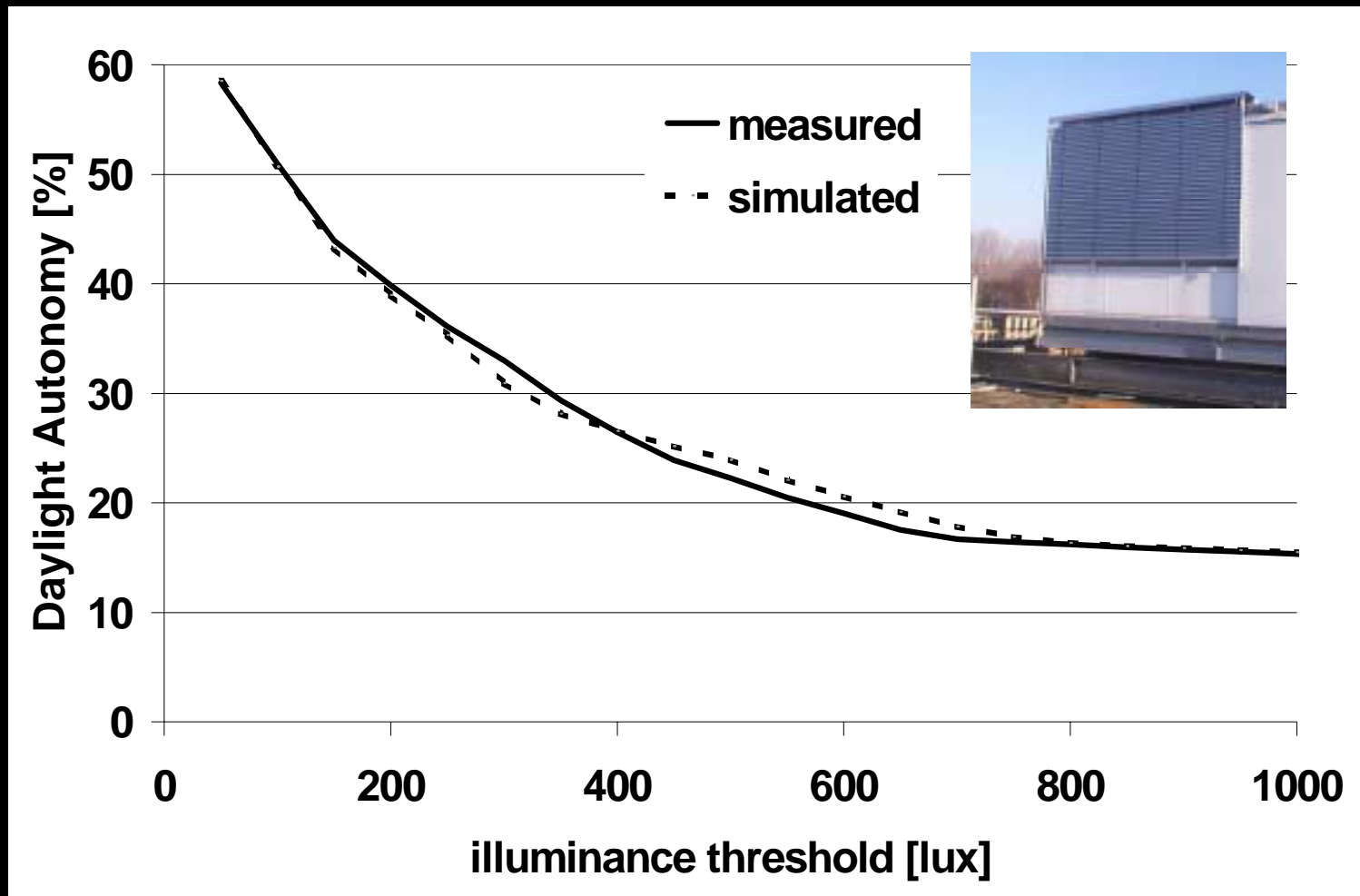
Reinhart & Herkel 2000



Daylight Coefficients were the fastest & most accurate dynamic method.

Previous Radiance Validation Studies

Energy & Buildings
Reinhart, Walkenhorst 2001



Radiance & Perez & Daylight Coefficients – venetian blinds

(Radiance materials: "plastic", "metal", "glass")

Conclusion from Previous Studies

- The combination Perez/Radiance/Daylight Coefficients is capable of accurately modeling the short time step development of indoor illuminances due to daylight for **complex geometries** and **"plastic"**, **"metal"**, and **"glass"** type materials.
- Good accuracy corresponds to a **MBE ~10%** and a **RMSE of ~25%**. The simulation errors for the sky model and the raytracing algorithm are of the same order of magnitude.
- Simulations of **ceiling sensors** tend to be **less accurate** (MBE ~20%, RMSE 30%) as they require detailed modeling of surrounding buildings and ground.

Validation Study: Objectives

- ❑ to increase the number of validated Radiance material modifiers to include **translucent glazings**,
- ❑ present a general methodology of how to derive a Radiance material model of a translucent panel based on **goniophotometer and integrating sphere measurements**, and
- ❑ to validate the resulting Radiance model in a **full scale test room**.

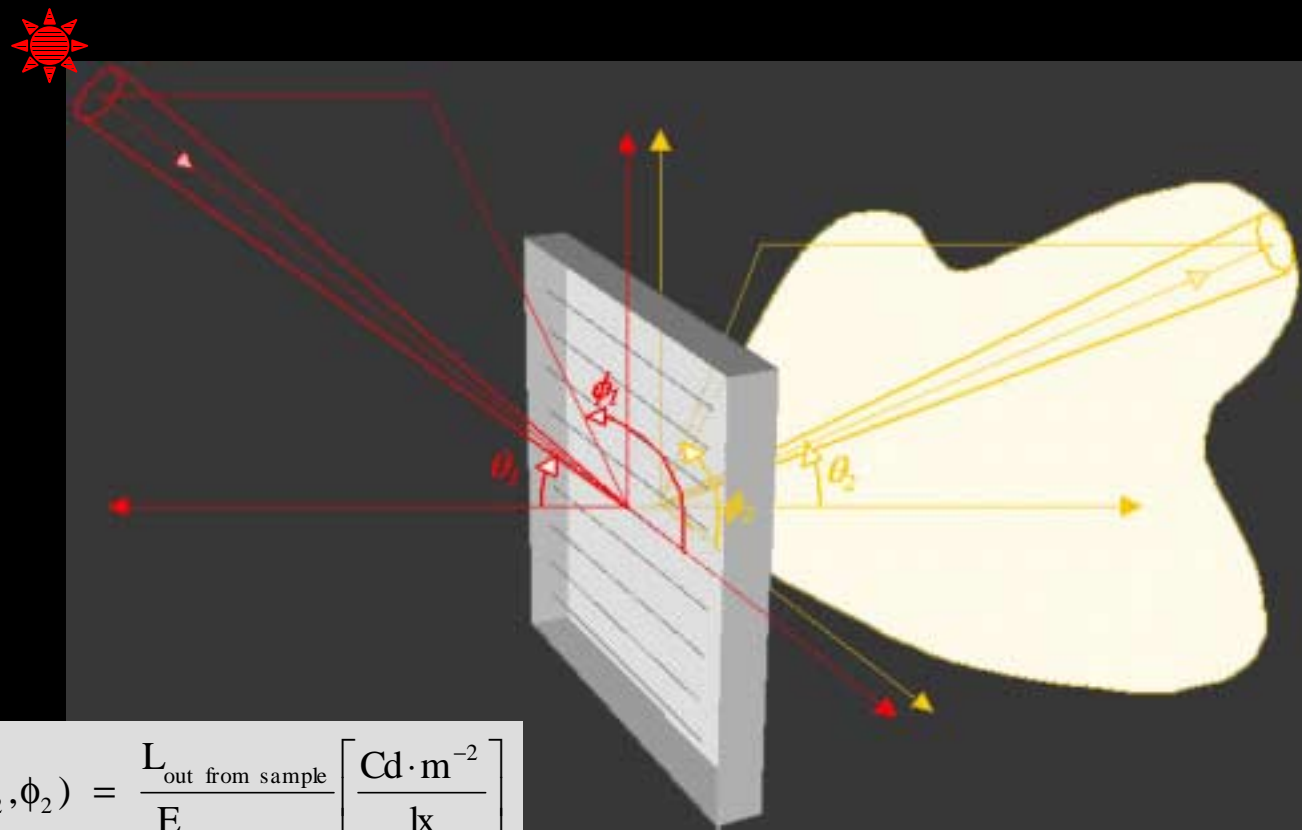
Kalwall Validation: Methodology

- Goniophotometer & Integrating Sphere Measurements
- Development of a Radiance model
- Test-room measurements
- Radiance/Perez validation

Goniophotometer measurements

Light redirecting systems assessment

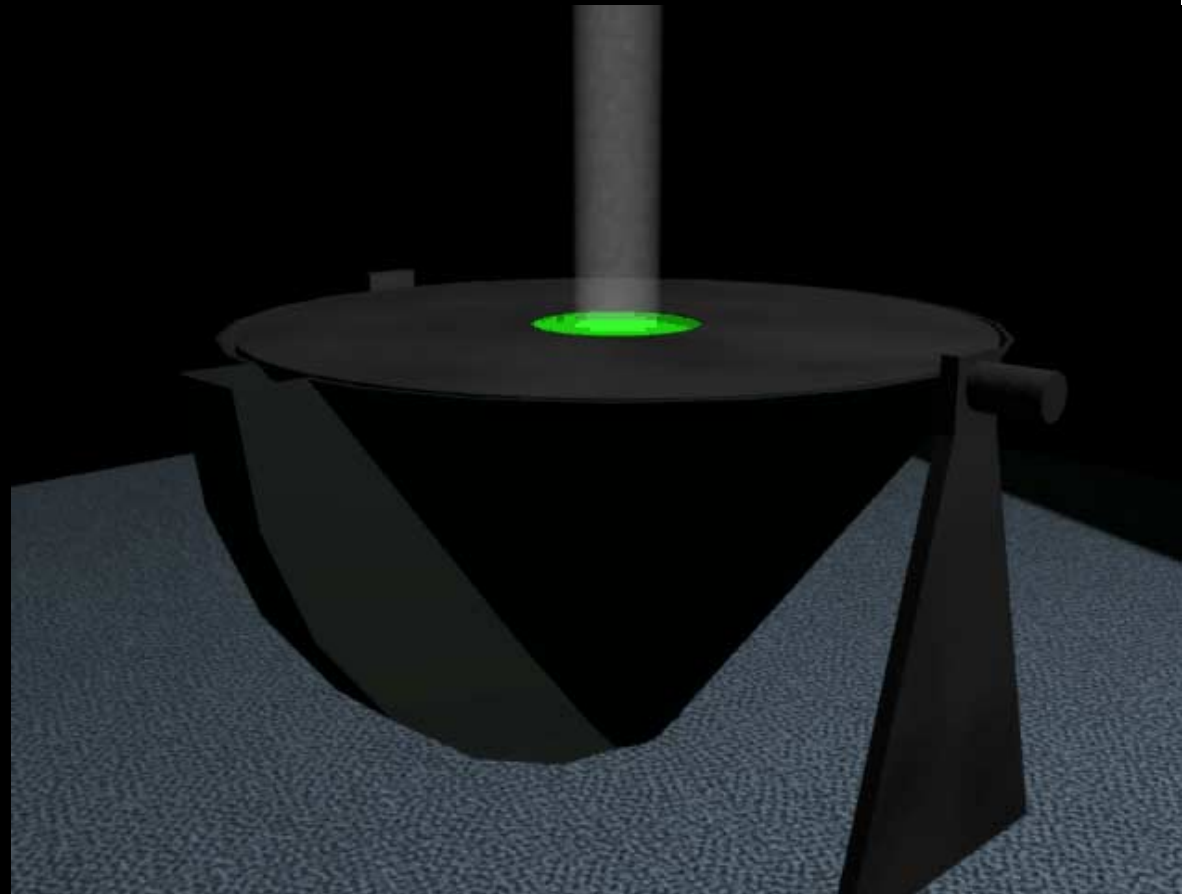
- BRDF or BTDF = light distribution after reflection or transmission, for each incident direction



$$\text{BT(R)DF}(\theta_1, \phi_1, \theta_2, \phi_2) = \frac{L_{\text{out from sample}}}{E_{\text{inc on sample}}} \left[\frac{\text{Cd} \cdot \text{m}^{-2}}{\text{lx}} \right]$$

EPFL bidirectional goniophotometer

- Functioning principle: Transmission



courtesy of M. Andersen

NRC-CARC

The Sample

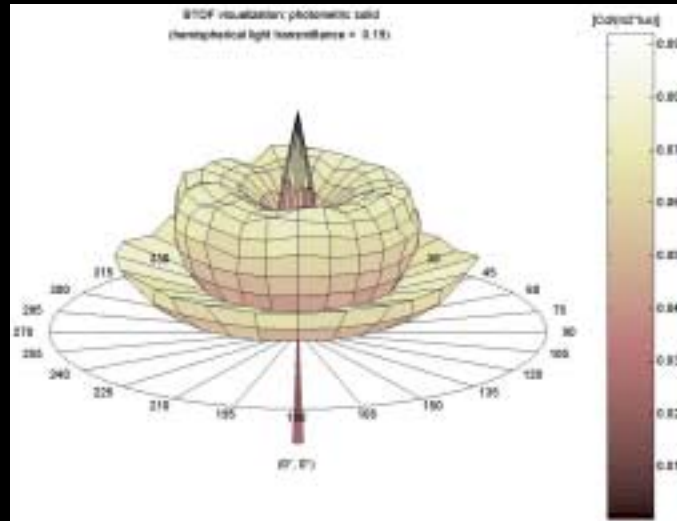


exterior

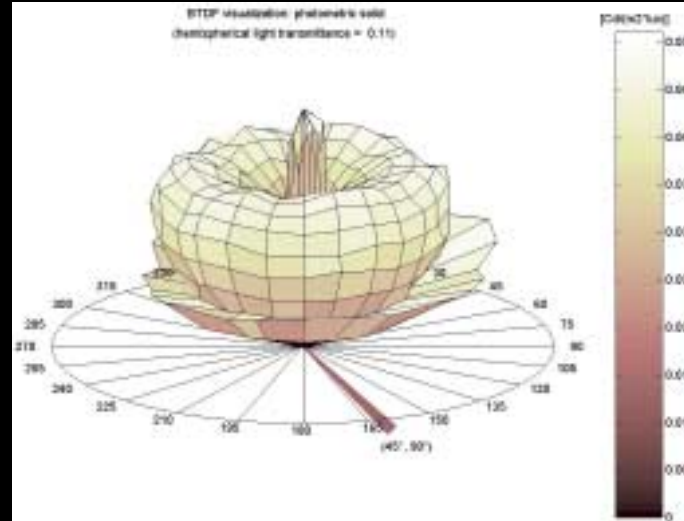


Interior

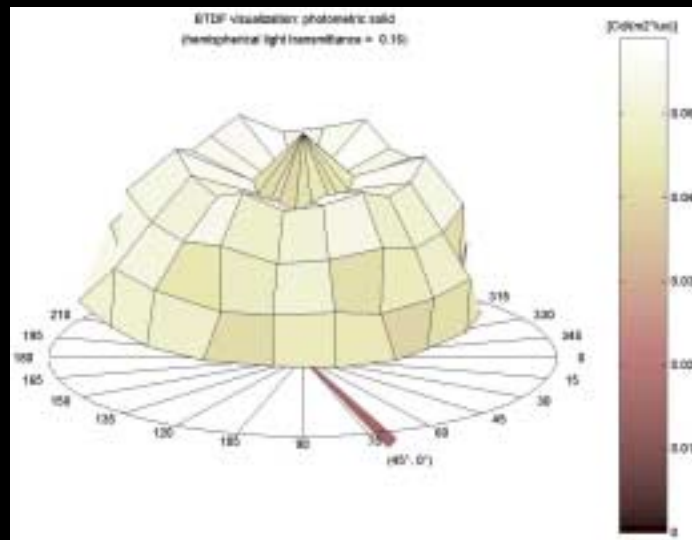
Goniophotometer Measurements I



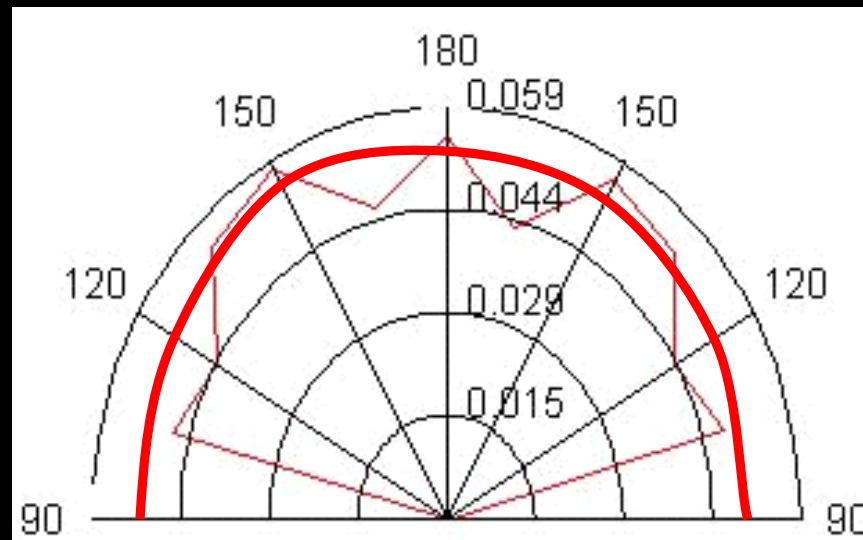
BTDF along $\theta_{\text{incident}}=0^\circ$, $\phi_{\text{incident}}=0^\circ$, $\varnothing = 150$ mm



BTDF along $45^\circ, 90^\circ$, $\varnothing = 150$ mm



BTDF along $45^\circ, 0^\circ$, $\varnothing = 280$ mm



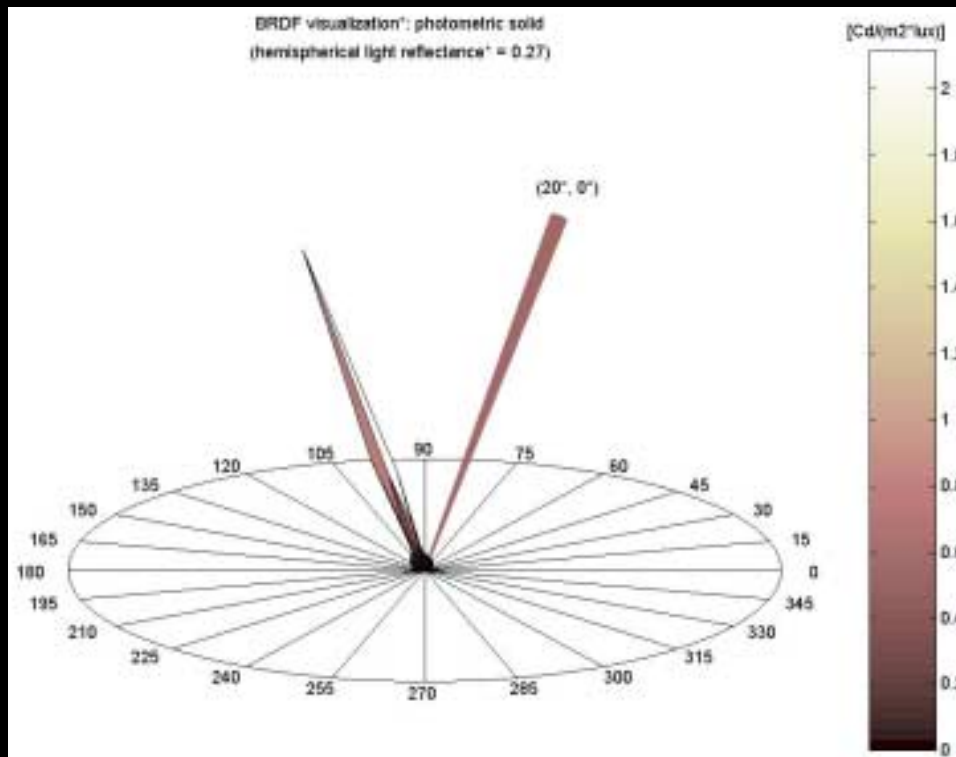
BTDF along $45^\circ, 0^\circ$ (section view), $\varnothing = 280$ mm

- two diaphragm sizes used: 150mm and 280mm (tradeoff between edge effects and signal to noise ratio)

Goniophotometer Measurements II

Approximation: The system is **rotationally invariant** (no variation with either the incident or the emerging azimuth angles).

The spatial heterogeneity in diffusion being due to the framing and size of the analyzed sample as well as to the limitations of the experimental equipment, the system can reasonably be **considered as a good diffuser**.



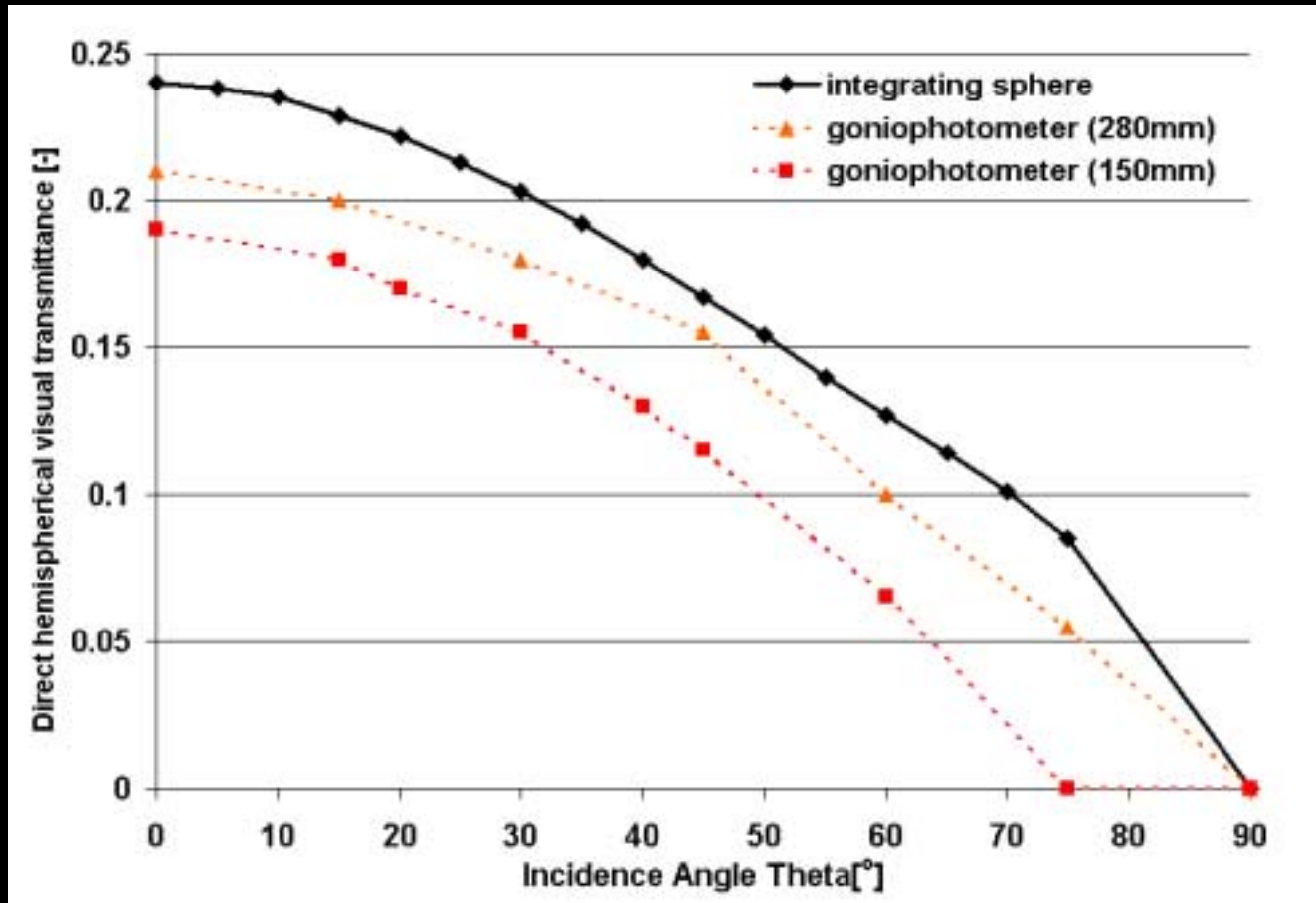
BRDF:

mean diffuse refl. 21%

specular refl. 8%

BRDF along 20°, 0°, $\varnothing = 150$ mm

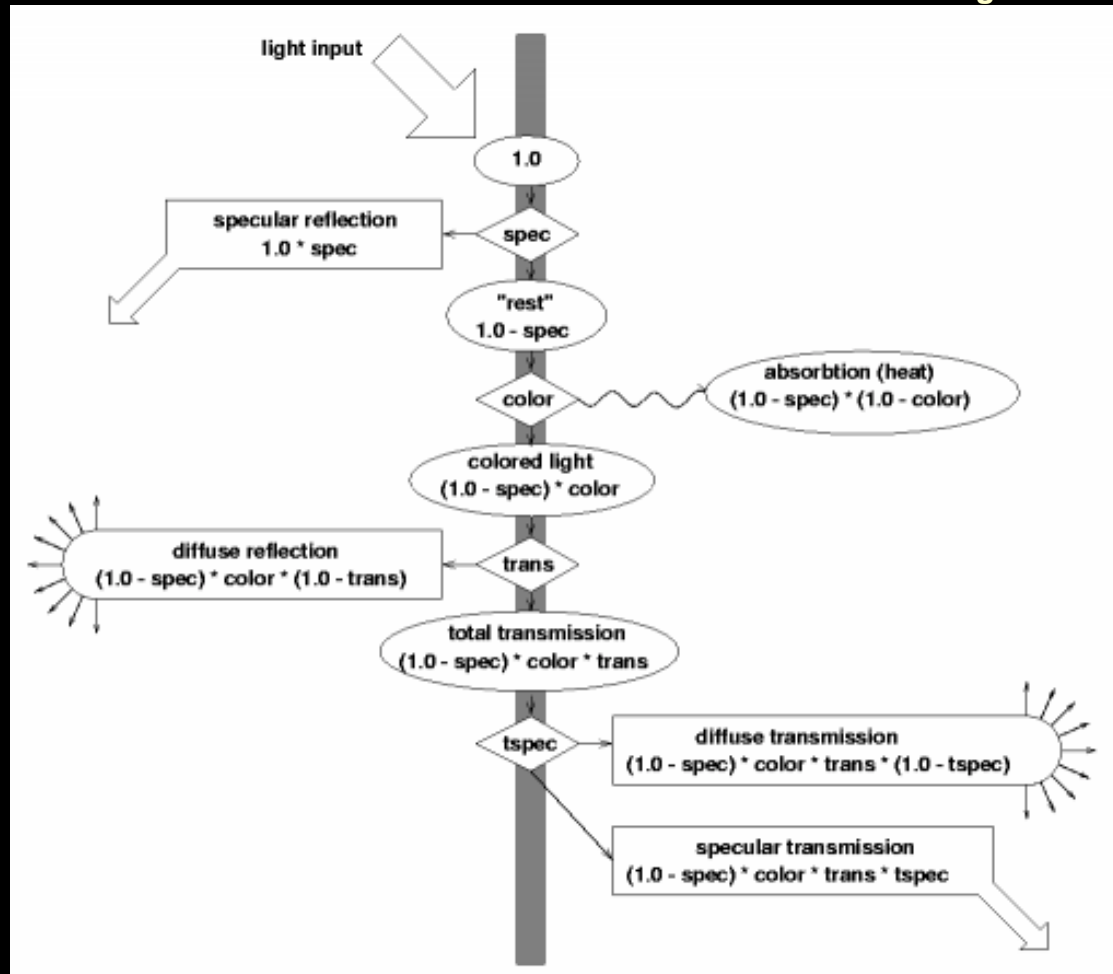
Direct hemispherical Transmittance



- an ideal diffuser would have a constant function.
- direct normal hemispherical transmittance 24%

“trans” and “transdata”

Website - Georg Mischler



- “trans” describes an ideal diffuser.
 - “transdata” allows to specify an angle dependant transmittance.
- Caveat:** The function files only apply to direct sunlight and not to diffuse daylight.

trans_{24%}

```
# RADIANCE "trans" model of a translucent panel assuming
# only direct normal hemispherical transmittance is available
#  $R_d = C_r = C_g = C_b = 0.21$  = diffuse reflectance
#  $R_s = A_4 = 0.08$  = specular reflectance
#  $S_r = 0.0$  = surface roughness
#  $T_d = 0.24$  = direct normal diffuse hemispherical transmittance
#  $T_s = 0$  = transmitted specularity (ideal diffuser)
#  $A_7 = T_s / (T_d + T_s) = 0$ 
#  $A_6 = (T_d + T_s) / (R_d + T_d + T_s) = 0.5333$ 
#  $A_5 = S_r = 0$ 
#  $A_1 = A_2 = A_3 = R_d / ((1 - R_s) * (1 - A_6)) = 0.48913$ 
#  $S_t = A_6 * A_7 * (1 - A_1) * A_4 = 0$ 
# resulting Radiance material:
void trans PANEL
0
0
7 0.48913 0.48913 0.48913 0.08 0 0.5333 0
# A1      A2      A3      A4      A5 A6      A7
```

trans_{16%}

```
# RADIANCE "trans" model of a translucent panel assuming
# only direct normal hemispherical transmittance is available
#  $R_d = C_r = C_g = C_b = 0.21$  = diffuse reflectance
#  $R_s = A_4 = 0.08$  = specular reflectance
#  $S_r = 0.0$  = surface roughness
#  $T_d = 0.16$  = diffuse - diffuse transmittance
#  $T_s = 0$  = transmitted specularity (ideal diffuser)
# ...
void trans PANEL
0
0
7 0.40446 0.40446 0.40446 0.08 0 0.435635 0
# A1      A2      A3      A4    A5 A6      A7
```

“transdata”

```
void transdata PANEL
4 noop refl.dat rang.cal rang
0
6 0.40446 0.40446 0.40446 0.08 0.435635 1
```

refl.dat

```
##### HEADER #####
# one-dimensional data array
1
# irregularly spaced axis:
# two zeros – number of divisions – division values
0 0 17
0 5 10 15 20 25 30 35 40 45 50 55 60 65 70 75 90
##### Body #####
# Data values:
0.471279687
0.467352356
0.46146136
0.449679368
0.43593371
0.418260722
0.398624068
0.377023749
0.353459765
0.327931838
0.302404466
0.274913151
0.249385501
0.223857851
0.198330201
0.166911556
0
```

rang.cal

```
{ Compute incident angle in degrees (from either side) }
rang(dx,dy,dz) = 180/PI*Acos(abs(Nx*dx+Ny*dy+Nz*dz));
```


Validation Measurements

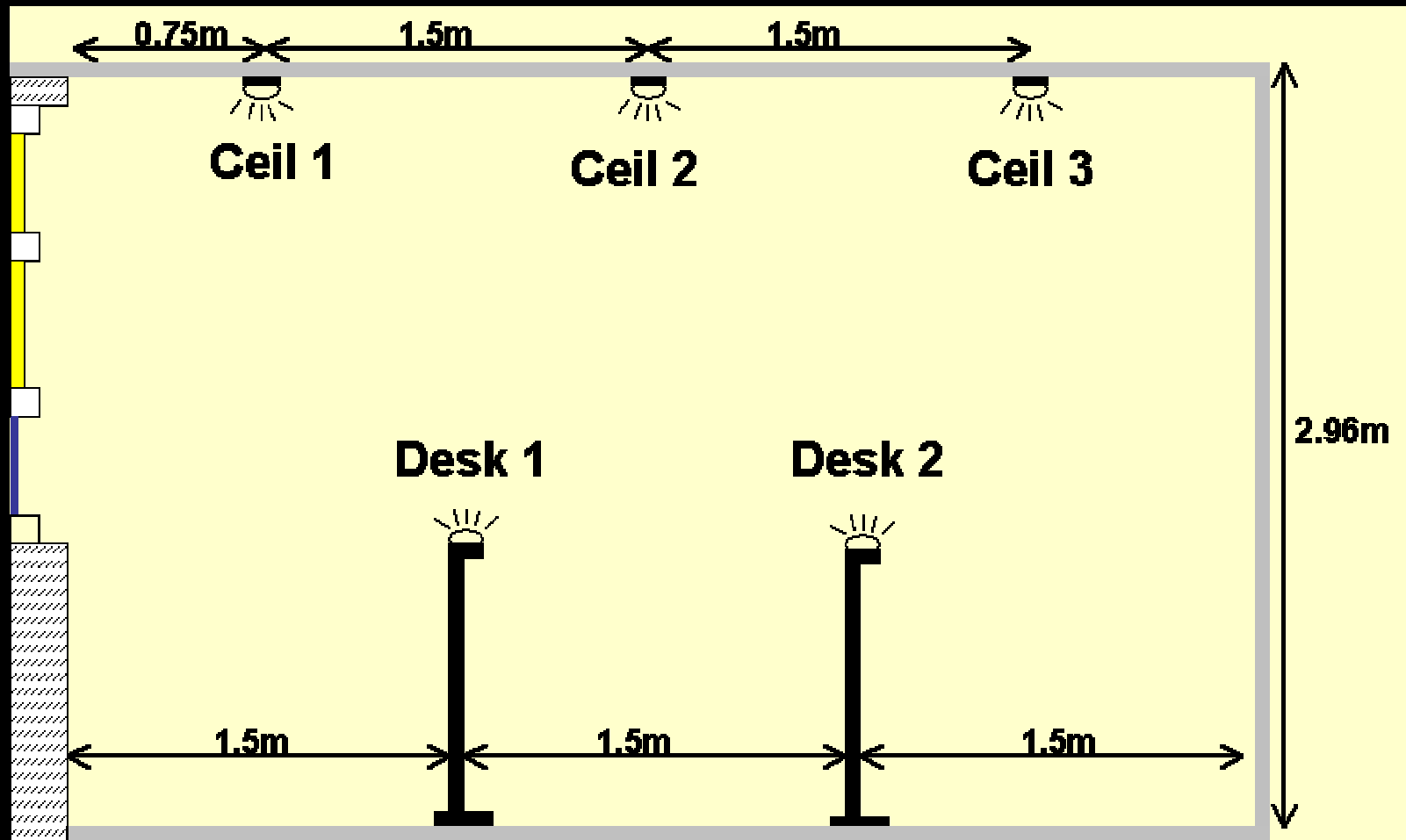


NRC Daylighting Lab



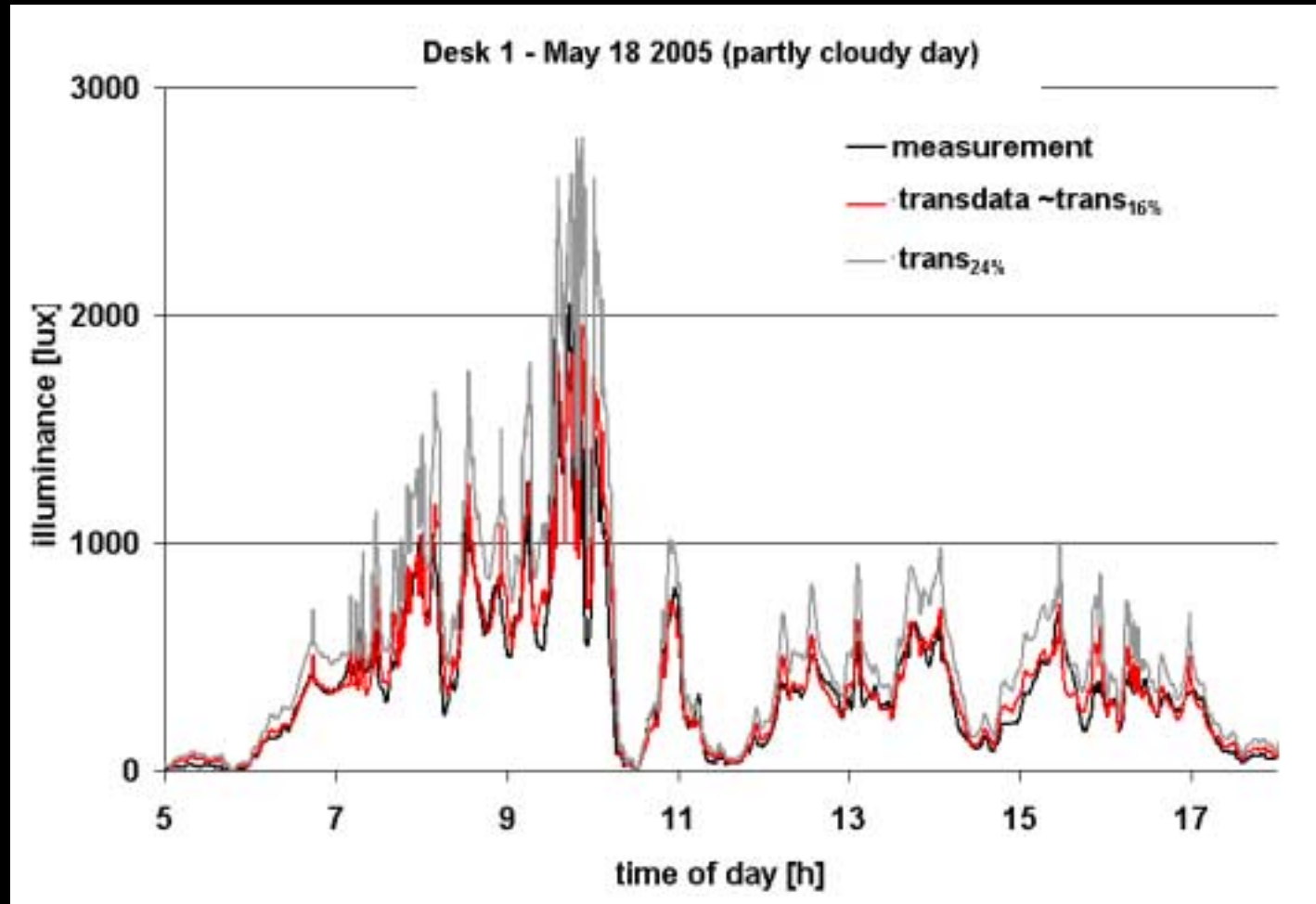
“hedge” with black cloth

Validation Measurements



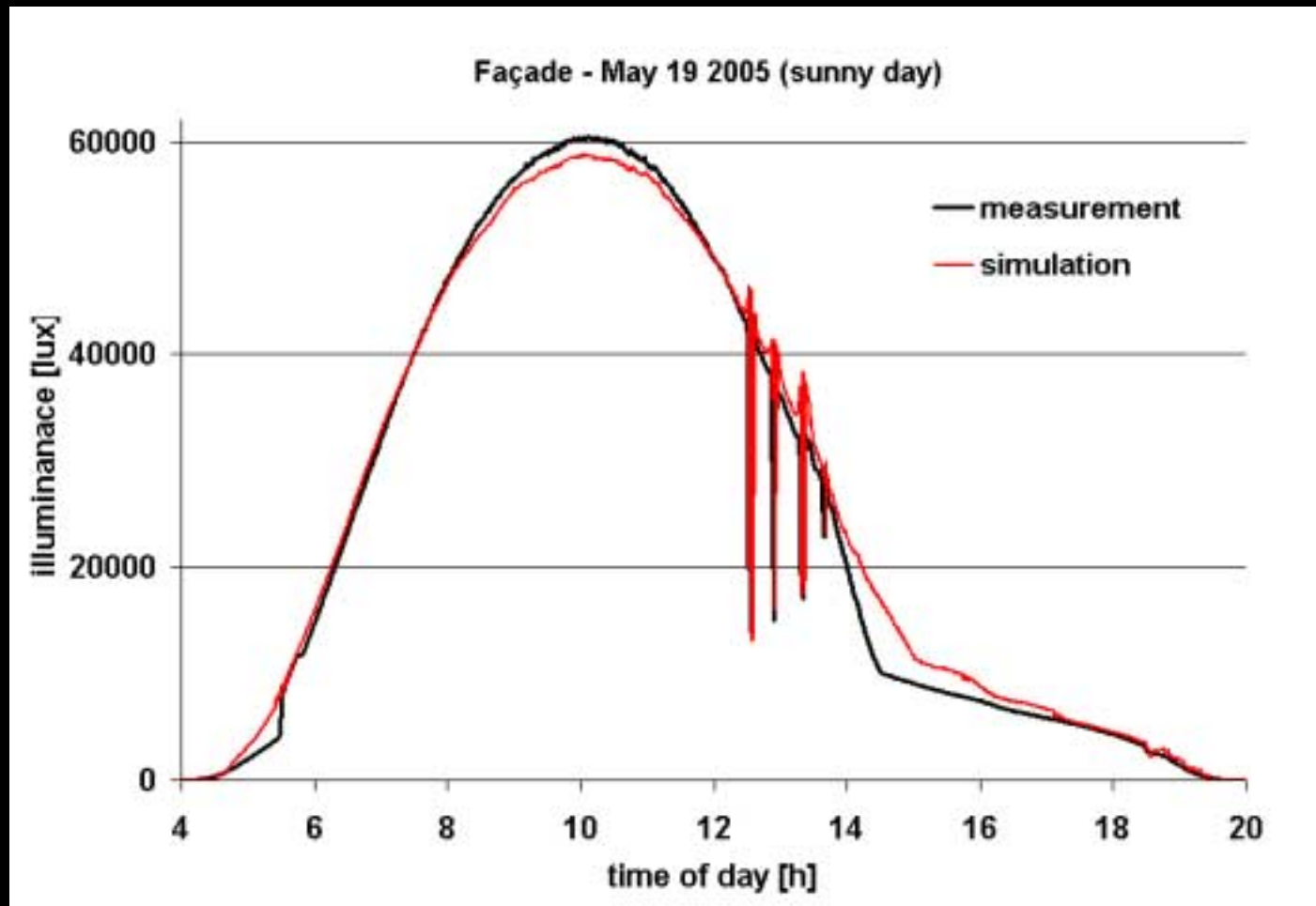
5 indoor illuminance sensors, 1 façade illuminance sensor, direct and diffuse irradiance... 19 days... 30 sec measurement interval...
>120,000 illuminance measurements

Partly Cloudy Day



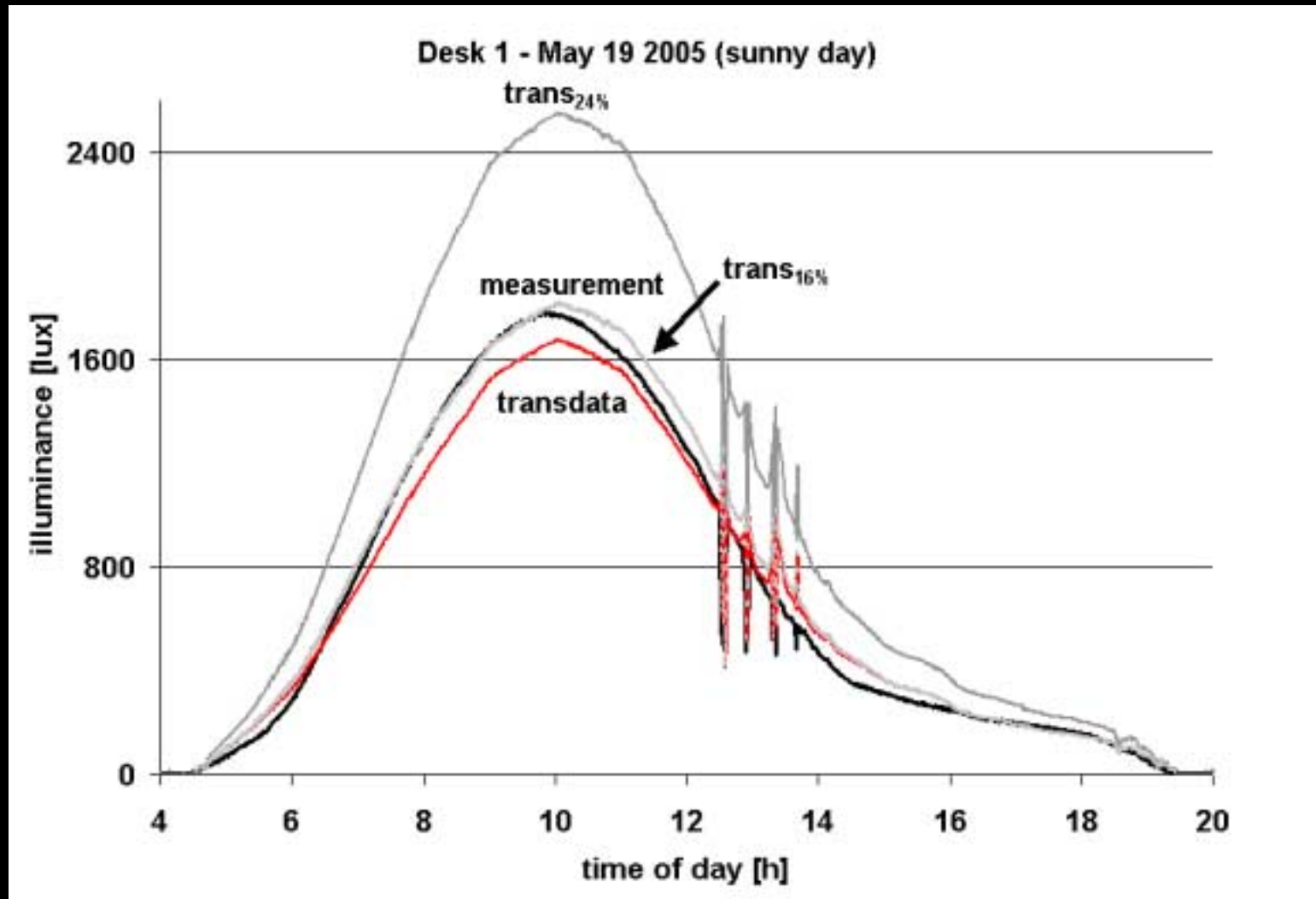
- excellent agreement
- “trans_{16%}” and “transdata” model nearly identical

Sunny Day - Outside



•

Sunny Day - Inside



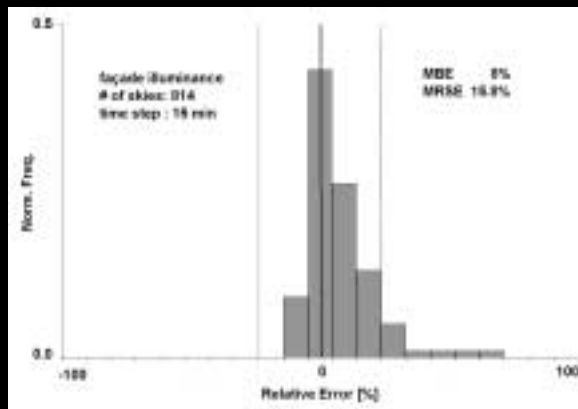
- "transdata" & "trans_{16%}" better than "trans_{24%}"

MBE & RMSE

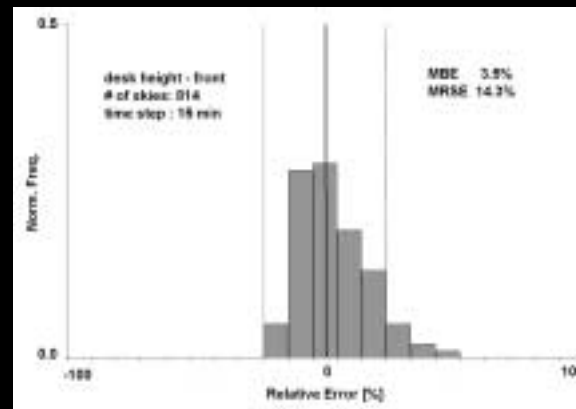
sensor		trans _{24%}	trans _{16%}	transdata
DESK1	MBE [%]	49.5	7.5	3.5
	RMSE [%]	52.4	14.6	14.3
CEIL1	MBE [%]	57.7	12.7	8.9
	RMSE [%]	60.9	19.2	18.6

Error Distribution Spectra Radiance & Perez

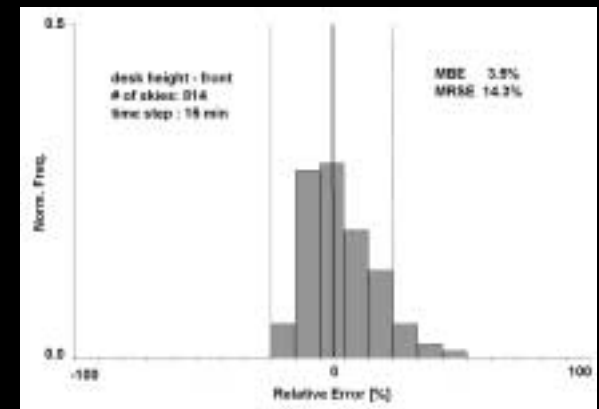
Facade



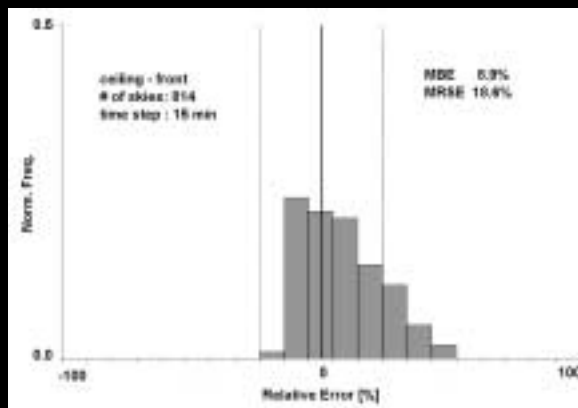
Desk 1



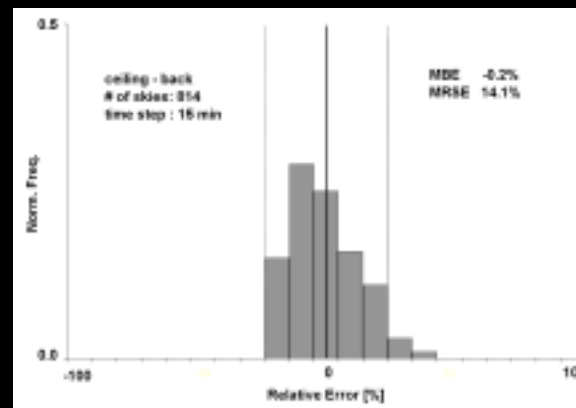
Desk 2



Ceil 1



Ceil 3

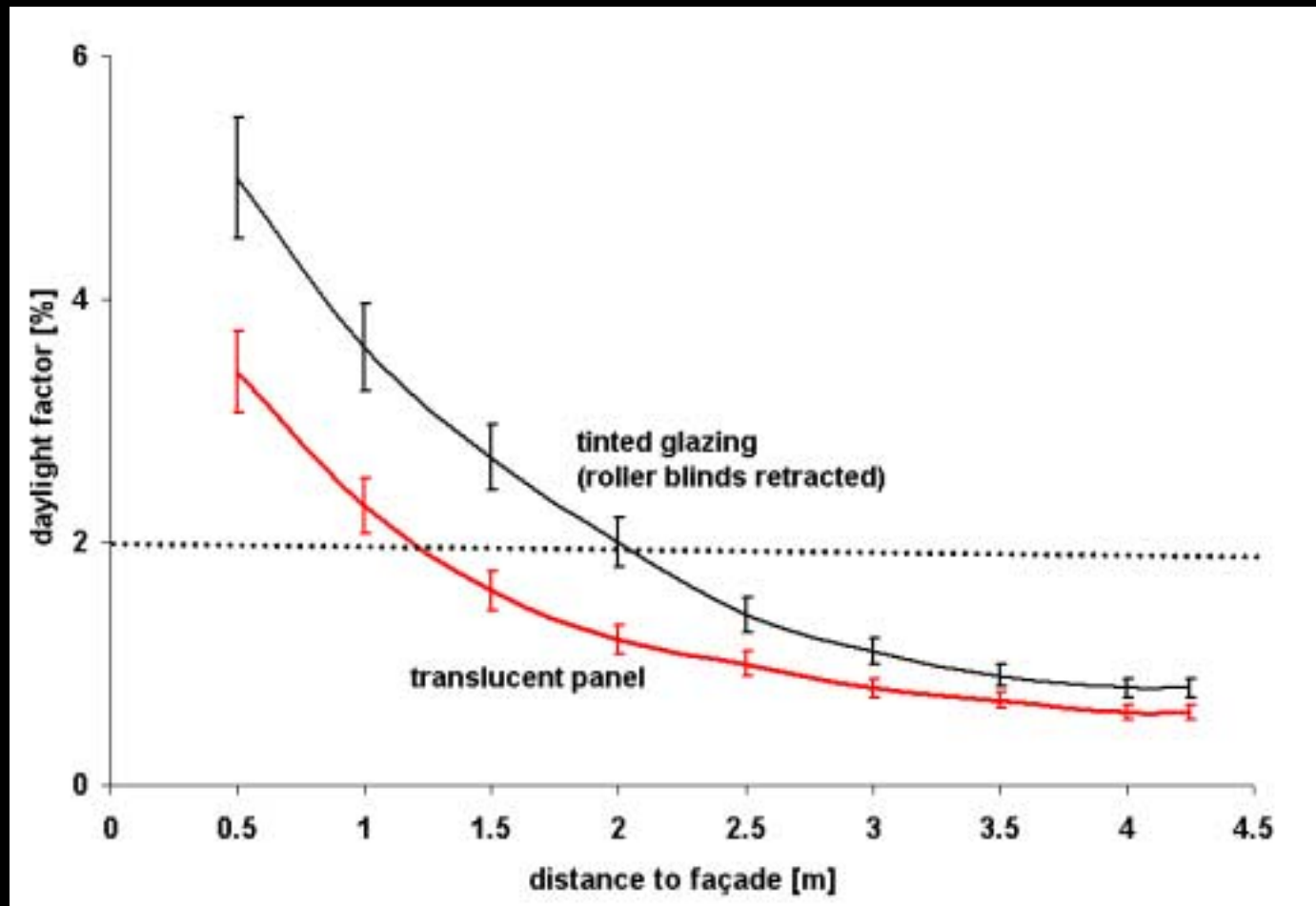


76% to 86% of simulations lie in 20% error band

Practical Considerations:

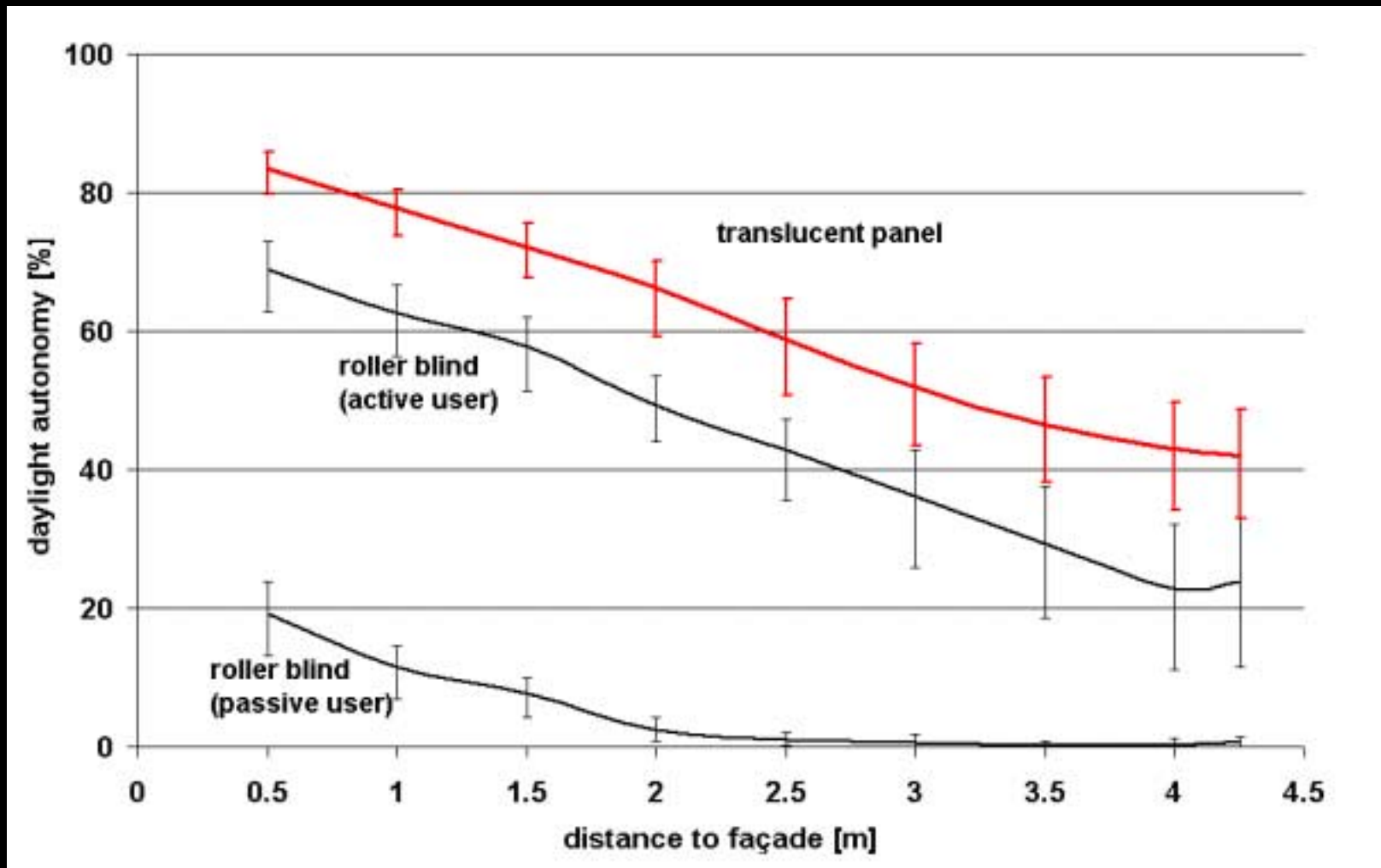
How significant is a 20% error?

Practical Considerations: Daylight Factor (10% error)



- 10% since no sky error
- Apply LEED analysis

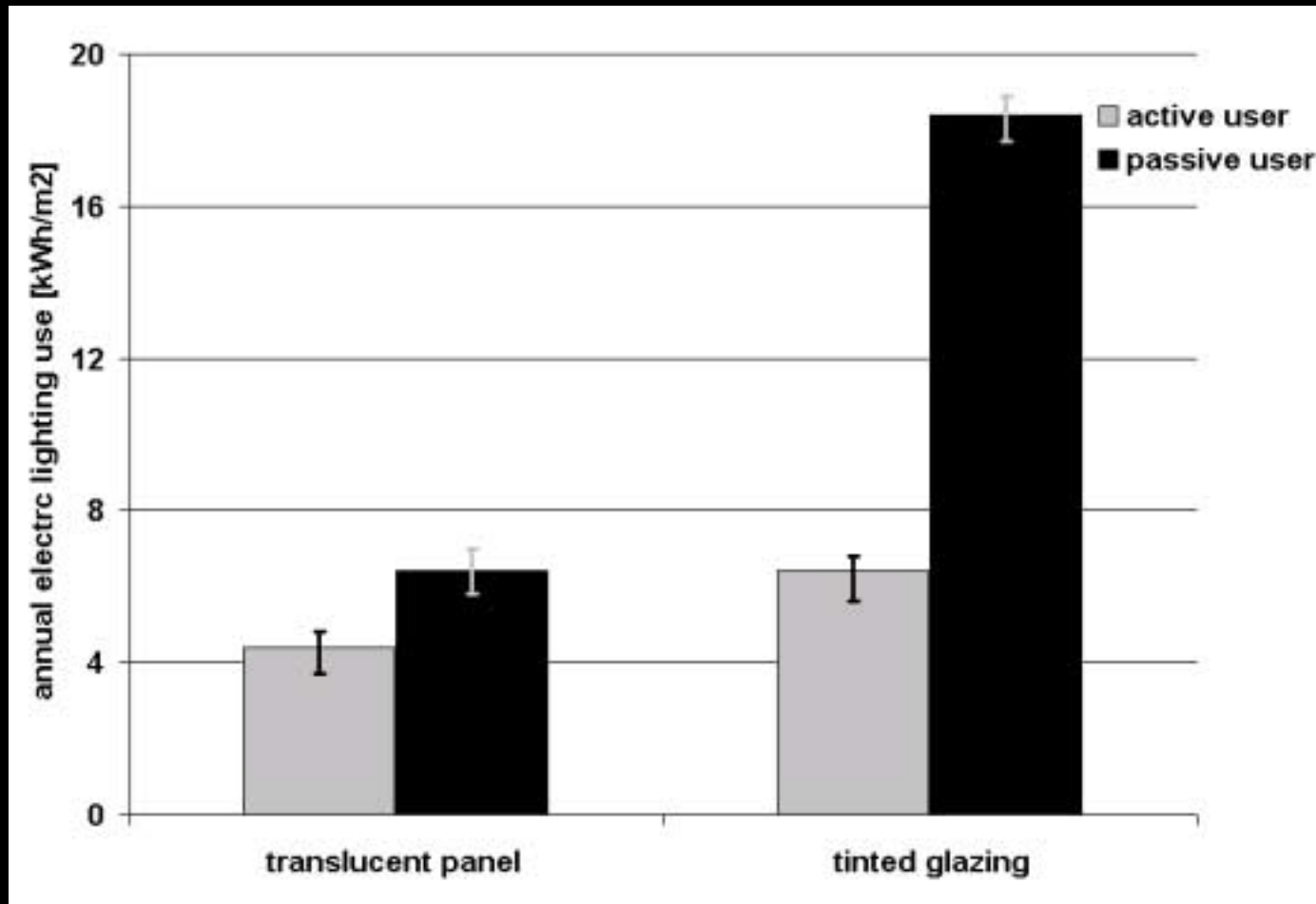
Practical Considerations: Daylight Autonomy (20% error)



Ottawa... Mo-Fr. 8.30 to 4.30... 450 lux min. ill...

Different results than DF analysis.

Practical Considerations: Electric Lighting Use (20% error)



- Ottawa... Mo-Fr. 8.30 to 4.30... 450 lux min. ill... **ideally photocell control**
- translucent panel always lower than tinted glazing with roller blinds.

Conclusion

- ❑ We now have a **validated Radiance model** of a translucent material (more to follow).
- ❑ Accuracy as good as in earlier studies for “glass”, “plastic”, and “metal”.
- ❑ Method developed **can be used for other materials** and products such as a photocell.